³Yang, S.-S., and Song, T.-H., "An Improved WSGGM-Based Narrow-Band Model for the CO₂ 4.3 µm Band," International Journal of Thermal Science, Vol. 38, No. 3, 1999, pp. 228–238.

⁴Soufiani, A., and Taine, J., "High Temperature Gas Radiative Property Parameters of Statistical Narrow-Band Model for H2O, CO2 and CO, and Correlated-K Model for H2O and CO2," International Journal of Heat and Mass Transfer, Vol. 40, No. 4, 1997, pp. 987-991.

⁵Lacis, A. A., and Oinas, V., "A Description of the Correlated k Distribution Method for Modeling Nongray Gaseous Absorption, Thermal Emission, and Multiple Scattering in Vertically Inhomogeneous Atmosphere," Journal of Geophysical Research, Vol. 96, No. D5, 1991, pp. 9027-9063.

⁶Goody, R., West, R., Chen, L., and Crisp, D., "The Correlated-k Method for Radiation Calculations in Nonhomogeneous Atmospheres," Journal of Quantitative Spectroscopy and Radiative Transfer, Vol. 42, No. 6, 1989, pp. 539-550.

⁷Liu, F., Smallwood, G. J., and Gülder, Ö. L., "Application of the Statistical Narrow-Band Correlated-k Method to Non-Grey Gas Radiation in CO2-H₂O Mixtures: Approximate Treatments of Overlapping Bands," Journal of Quantitative Spectroscopy and Radiative Transfer (submitted for publica-

⁸Liu, F., Smallwood, G. J., and Gülder, Ö. L., "Application of the Statistical Narrow-Band Correlated-k Method to Low-Resolution Spectral Intensity and Radiative Heat Transfer Calculations—Effects of the Quadrature Scheme," International Journal of Heat and Mass Transfer (to be published).

⁹Marin, O., and Buckius, R. O., "A Model of the Cumulative Distribution Function for Wide Band Radiative Properties," Journal of Quantitative

Spectroscopy and Radiative Transfer, Vol. 59, No. 6, 1998, pp. 671-685. ¹⁰Kim, T.-K., Menart, J. A., and Lee, H. S., "Nongray Radiative Gas Analysis Using the S-N Discrete Ordinates Method," Journal of Heat Transfer, Vol. 113, No. 4, 1991, pp. 946-952.

Non-Fourier Heat-Flux Law for Diatomic Gases

Abdulmuhsen H. Ali* Kuwait University, Safat 13060, Kuwait

Nomenclature

$E^{\rm int}(v,r)$	= internal energy of the reduced mass
$E^{\rm kin}(v)$	= kinetic part of the internal energy
$E^{\mathrm{pot}}(r)$	= potential part of the internal energy
$E^{\mathrm{tr}}(V)$	= translational energy of the center of mass
E(V, v, r)	= total energy, $E^{tr}(V) + E^{int}(v, r)$
$\{\hat{e}_l\}$	= set of linearly independent basis
$f^{(1)}(\boldsymbol{R}, \boldsymbol{V}, t)$	= local equilibrium distribution function
	for the center of mass:
	$n_M(\mathbf{R},t)[M\beta(\mathbf{R},t)/2\pi]^{\frac{3}{2}}$

$$\times \exp\{-[M\beta(\mathbf{R},t)/2][V-\mathbf{u}_M(\mathbf{R},t)]^2\}$$

$$f^{(1)}(\mathbf{R}, \mathbf{v}, t)$$
 = local equilibrium distribution function for the reduced mass:

$$n_{\mu}(\mathbf{R}, t) \left[\mu \beta(\mathbf{R}, t) / 2\pi\right]^{\frac{3}{2}}$$

$$\times \exp\left\{-\left[\mu \beta(\mathbf{R}, t) / 2\right] \left[\mathbf{v} - \mathbf{u}_{\mu}(\mathbf{R}, t)\right]^{2}\right\}$$

$g(\mathbf{r})$	= radial or pair distribution function, $\exp[\beta W(r)]$
$\boldsymbol{J}(t)$	= heat flux
k_B	= Boltzmann constant
M	= total mass of the diatomic molecule

Received 10 September 1999; revision received 16 November 1999; accepted for publication 16 November 1999. Copyright © 2000 by the American Institute of Aeronautics and Astronautics, Inc. All rights reserved.

$n_M(\mathbf{R},t)$	= number density of the total mass
$n_{\mu}(\boldsymbol{R},t)$	= number density of the reduced mass
ĥ	= unit vector
q	= real number
R	= position vector of the center of mass
r	= position vector of the relative distance
	between two point particles
r_m	= distance between point particles at which their
	potential energy is minimum
T	= temperature
t	= time
$\boldsymbol{u}_{M}(\boldsymbol{R},t)$	= center-of-mass average velocity vector, $\langle V \rangle$
$\boldsymbol{u}_{\mu}(\boldsymbol{R},t)$	= reduced-mass average velocity vector, $\langle v \rangle$
V	= velocity of the center of mass
ν	= velocity of the relative position vector
	between two point particles
W(r)	= potential energy of the average force
	a particle experiences
β	$= 1/k_BT$
$eta^*_{ m dia}$	= Eucken number for diatomic gases:
	$\left[{}_{B^*} - \frac{(5-3\gamma)}{6} {}_{B^*} \right]$

 $\beta_{\rm tr}^* - \frac{(3-37)}{3(\gamma-1)}\beta_{\rm int}^*$

= Eucken number caused by internal states:

$$3\left[1 - \frac{\mu(\delta v)^2}{3k_B T} + \frac{2\langle E^{\text{int}}W(r)\rangle}{3\langle E^{\text{int}}\rangle k_B T}\right]$$

$eta_{ ext{tr}}^*$	= Eucken number caused by translational motion,
u	$3[1-M(\delta V)^2/3k_BT]$
Γ	= arbitrary volume over which the relative
	coordinate is integrated
γ	= ratio of heat capacities
Δ	= variable's nonequilibrium instantaneous
	departure from its equilibrium value
Δa	= total area:
	Α.

δ	= fluctuation in a variable
∂_t	= derivative with respect to time, $\partial/\partial t$
ϵ	= perturbation
θ	= time as an integration variable
λ	= thermal conductivity of diatomic gases,
	$\beta_{\rm dia}^* \langle E^{\rm tr} \rangle u / 2T \Delta a$
λ_{int}	= thermal conductivity caused by internal motion,
	$\beta_{\rm int}^* \langle E^{\rm int} \rangle u / 2T \Delta a$
λ_{tr}	= thermal conductivity caused by translational
	motion, $\beta_{tr}^* \langle E^{tr} \rangle u / 2T \Delta a$
μ	= reduced mass of the diatomic molecule
σ	= physical constant, $\beta_{dia}^* \langle E^{tr} \rangle / 3\Delta a$
τ	= relaxation time
()	= nonequilibrium ensemble average
$\langle \rangle_e$	= equilibrium ensemble average

Introduction

PREVIOUSLY a derivation of the Cattaneo's heat-flux law, which is a non-Fourier back of $which is a non-Fourier heat-flux\ law, was\ given for\ monoatomic$ gases. The derivation of Cattaneo's heat-flux equation for diatomic gases will emphasize the validity of the method used before for monoatomic gases, which is an important thing to do before the method is applied to the far-from-equlibrium case, and will demonstrate the phenomenon of finite speed heat propagation for a different kind of gas, namely the diatomic gas. Therefore, the derivation of Cattaneo's heat-flux equation for diatomic gases is presented here. Under special conditions, which include being at the critical temperature, the method used before proved very successful here in the case of diatomic gases. However, the distribution function that

^{*}Assistant Professor, Department of Physics, P.O. Box 5969; alie@kuc01. kuniv.edu.kw.

corresponds to the diatomic gas is taken as a product between the distribution function of the total mass of the diatomic molecule, the distribution function of the reduced mass of the diatomic molecule, and a function that represents the radial distribution function.² Pair distribution functions in the form of a product between two distribution functions representing each particle and a radial distribution function have been extensively used before³ and were mainly used to study correlations.⁴ When the radial distribution function equals unity for all values of the radial distances between the two particles, one gets the Vlasov equation, which resembles the collisionless Boltzmann equation.⁵ Sometimes the correct form of the pair distribution function is reached a posteriori, depending on the final numerical results.³ Writing the pair distribution function in a product form has been applied in this Note because of the nature of diatomic molecules. Moreover, when a diatomic gas at the critical temperature is considered here, the value of the Eucken number will be 1.875 in comparison to the value obtained by Eucken (see Ref. 6), which is 1.94.

Derivation of Cattaneo's Heat Flux for Diatomic Gases

In the case of diatomic molecules, one must write the energy as $^2E=E^{\rm tr}+E^{\rm int}$. For a constant value of γ , the two energies at equilibrium are related by 7

$$\langle E^{\rm int} \rangle_e = \frac{(5 - 3\gamma)}{3(\gamma - 1)} \langle E^{\rm tr} \rangle_e \tag{1}$$

and because local equilibrium is considered here, Eq. (1) can be applied. The relation $E^{\rm int} = [(5-3\gamma)/3(\gamma-1)]E^{\rm tr}$ can be immediately reached from Eq. (1). The equation for heat flux is written as $J = EV = (E^{\rm tr} + E^{\rm int})V$, which with the preceding relation can be written as $J(t) = [1 + (5-3\gamma)/3(\gamma-1)]E^{\rm tr}V(t)$. For diatomic gases $\gamma = 1.4$. In view of the fact that, for bound states, which resemble diatomic molecules, the internal energy is negative,⁷ the equation for the heat flux per unit volume will be given by

$$J(t) = \frac{1}{2} [MV^2(t)/2] V(t)$$

where V = |V|. With the aid of the Onsager hypothesis, the following equation can be obtained:

$$\langle \Delta \boldsymbol{J}(t) \rangle = \langle \boldsymbol{J}(t) \rangle = \frac{\beta \epsilon}{3} \sum_{t=1}^{3} \langle \delta \boldsymbol{J}(0) \cdot \delta \boldsymbol{J}(t) \rangle_{e} \hat{e}_{t}$$

$$\leq \beta \epsilon \left(\frac{M}{6}\right)^2 \frac{1}{3} \sum_{l=1}^3 \sum_{i=1}^3 \langle V_i(0)V_i(t) \rangle_e^3 \hat{e}_l \tag{2}$$

which is true at all times, where it is assumed that $\epsilon \propto \nabla T$. The conservation of energy equation can be written as¹

$$\int_{0}^{t} d\theta J(V, v, \theta) \cdot \Delta a = -E(V, v)$$
(3)

After taking the statistical average corresponding to a pair of particles, one gets

$$\int_{0}^{t} d\theta \langle \boldsymbol{J}(\boldsymbol{R}, \theta, t) \rangle \cdot \Delta \boldsymbol{a} = -\langle E(\boldsymbol{R}, t) \rangle$$
 (4)

where the average is taken using the pair distribution function given by $f^{(2)}(\pmb{R},\pmb{V},\pmb{r},\pmb{v},t)=f^{(1)}(\pmb{R},\pmb{V},t)f^{(1)}(\pmb{R},\pmb{v},t)g(|\pmb{r}|)$. Therefore,

$$\langle E(\mathbf{R}, t) \rangle = \frac{1}{2n} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \int_{\Gamma} d^3r \, d^3V \, d^3v E(V, v, r)$$

$$\times f^{(2)}(\mathbf{R}, V, \mathbf{r}, v, t)$$
(5)

where $n_M = n_\mu = n$. Setting $W(r) = W(r_m)$ and assuming the relation

$$E^{\text{int}}(v, r_m) = E^{\text{int}}(v) \exp[\beta W(r_m)], \qquad \int_{\Gamma} d^3 r g(r_m) = \frac{1}{n}$$

(see Appendix), the right-hand side of Eq. (5) is written as

$$2\langle E(\boldsymbol{R}, t) \rangle = \int_{-\infty}^{+\infty} d^{3}V \left(\frac{M\beta}{2\pi}\right)^{\frac{3}{2}} E^{\text{tr}}(V)$$

$$\times \exp\left\{-\frac{\beta M}{2\pi} [\boldsymbol{V} - \boldsymbol{u}_{M}(\boldsymbol{R}, t)]^{2}\right\} + \int_{-\infty}^{+\infty} d^{3}v \left(\frac{\mu\beta}{2\pi}\right)^{\frac{3}{2}} E^{\text{int}}(v)$$

$$\times \exp\left\{-\frac{\beta\mu}{2\pi} [\boldsymbol{v} - \boldsymbol{u}_{\mu}(\boldsymbol{R}, t)]^{2}\right\} \exp[\beta W(r_{m})] \tag{6}$$

It can be shown,¹ from Eq. (2), that after taking ∂_t of Eq. (4) one can get

$$\left[\int_{0}^{\tau} \partial_{t} \langle \boldsymbol{J}(\boldsymbol{R}, \theta, t) \rangle \, \mathrm{d}\theta + \langle \boldsymbol{J}(\boldsymbol{R}, t, t) \rangle \right] \cdot \Delta \boldsymbol{a} = -\partial_{t} \langle E(\boldsymbol{R}, t) \rangle \quad (7)$$

where the energies in Eq. (7) are twice as much as the energies in Eq. (4). A direct evaluation of the right-hand side of Eq. (7) will give

$$\begin{split} \partial_t \langle E(\boldsymbol{R}, t) \rangle &= \langle E^{\text{tr}}(V) \frac{3}{2} (M/2\pi) (2\pi/M\beta) \partial_t \beta \rangle \\ &+ \langle E^{\text{int}}(v) \frac{3}{2} (\mu/2\pi) (2\pi/\mu\beta) \partial_t \beta \rangle \\ &+ \langle \beta M E^{\text{tr}}(V) [\boldsymbol{V} - \boldsymbol{u}_M(\boldsymbol{R}, t)] \cdot \partial_t \boldsymbol{u}_M \rangle \\ &- \langle E^{\text{tr}}(V) (M/2) [\boldsymbol{V} - \boldsymbol{u}_M(\boldsymbol{R}, t)]^2 \partial_t \beta \rangle \\ &+ \langle \beta \mu E^{\text{int}}(v) [\boldsymbol{v} - \boldsymbol{u}_\mu(\boldsymbol{R}, t)] \cdot \partial_t \boldsymbol{u}_\mu \rangle \\ &- \langle E^{\text{int}}(v) (\mu/2) [\boldsymbol{v} - \boldsymbol{u}_\mu(\boldsymbol{R}, t)]^2 \partial_t \beta \rangle + \langle E^{\text{int}}(v) (\partial_t \beta) W(r_m) \rangle \end{split}$$

The Euler equation for the evolution of the temperature T is given by

$$\partial_t T = -\mathbf{u} \cdot \nabla T - 2T(\nabla \cdot \mathbf{u})/3$$

where $\mathbf{u} = n_M M \mathbf{u}_M(\mathbf{R}, t) + n_\mu \mu \mathbf{u}_\mu(\mathbf{R}, t) / (n_M M + n_\mu \mu)$ is the stream velocity. The evolution of β will be given by

$$\partial_t \beta = (1/k_B T^2) \boldsymbol{u} \cdot \nabla T + (1/k_B T^2) \frac{2}{3} (T \nabla \cdot \boldsymbol{u})$$
 (9)

The following equalities can be justified¹: $\langle E^j(V^j)V^j\rangle = \langle E^j(V^j)\rangle\langle V^j\rangle$ and $\langle E^j(V^j)^2\rangle = \langle E^j\rangle\langle (V^j)^2\rangle$, where the index j runs over the translational and the internal modes. These equalities will furnish the following equations:

$$\langle E^{j} \left[\mathbf{V}^{j} - \mathbf{u}_{j}(\mathbf{R}, t) \right] \rangle = 0 \tag{10}$$

$$\langle E^{j}(V^{j}) [V^{j} - \mathbf{u}_{j}(\mathbf{R}, t)]^{2} \rangle = \langle E^{j} \rangle [\langle (V^{j})^{2} \rangle - \langle V^{j} \rangle^{2}]$$

$$= \langle E^{j} \rangle (\delta V^{j})^{2}$$
(11)

Substitution of the equalities in Eqs. (9–11) into Eq. (8) gives

$$-\partial_t \langle E(\mathbf{R}, t) \rangle = -\left(\frac{\beta_{\text{tr}}^* \langle E^{\text{tr}} \rangle}{2T} + \frac{\beta_{\text{int}}^* \langle E^{\text{int}} \rangle}{2T}\right) \mathbf{u} \cdot \nabla T$$

$$-\frac{1}{3}\left(\beta_{tr}^*\langle E^{tr}\rangle + \beta_{int}^*\langle E^{int}\rangle\right)\nabla \cdot \boldsymbol{u} \tag{12}$$

From Eq. (1) one can write the local equilibrium equation $\langle E^{\text{int}} \rangle = [(5-3\gamma)/3(\gamma-1)] \langle E^{\text{tr}} \rangle$, which, when substituted into Eq. (12) together with Eq. (7), yields

$$\int_{0}^{t} \partial_{t} \langle \boldsymbol{J}(\boldsymbol{R}, \theta, t) \rangle d\theta + \langle \boldsymbol{J}(\boldsymbol{R}, t, t) \rangle = -(\lambda_{\text{tr}} + \lambda_{\text{int}}) \nabla T$$

$$-\frac{\beta_{\text{dia}}^{*} \langle E^{\text{tr}} \rangle}{3 \wedge a} \hat{n} (\nabla \cdot \boldsymbol{u})$$
(13)

$$\int_{0}^{\tau} \partial_{t} \langle J(\mathbf{R}, \theta, t) \rangle d\theta + \langle J(\mathbf{R}, t, t) \rangle = -\lambda \nabla T - \sigma \hat{n} (\nabla \cdot \mathbf{u}) \quad (14)$$

where $E^{\text{int}} = -|E^{\text{int}}|$ for bound states.⁷ With the use of Ergodic theory,1 Eq. (14) will immediately lead to

$$\tau \frac{\partial \langle \boldsymbol{J}(\boldsymbol{R},t) \rangle}{\partial t} + \langle \boldsymbol{J}(\boldsymbol{R},t,t) \rangle = -\lambda \nabla T - \sigma \hat{n} (\nabla \cdot \boldsymbol{u})$$
 (15)

which is the non-Fourier heat-flux law for diatomic gases, given that the gas is incompressible. If Eq. (1) is used in the equation for β_{int}^* and the assumption that $W(r_m)$ and $\langle E^{\text{tr}} \rangle$ are uncorrelated is applied, one gets $\beta_{\text{int}}^* = 3\{1 - [\mu(\delta v)^2/3k_BT] + 2W(r_m)/3k_BT\}$. Furthermore, because the pair correlation has a single maximum for low densities that occurs at r_m for the Lennard-Jones potential,⁵ which represents gases, one may substitute the value of the Lennard-Jones potential² at r_m for $W(r_m)$. Then, assuming it to be at the critical temperature, one gets the equation $W(r_m) = -0.77k_BT_c$, where the minus sign is caused by the fact that the bound state is con- $(8/\pi) = 2.547$, and $\beta_{\rm dia}^* = 2.547 - 0.667(1.007) = 1.875$ at $T = T_c$, where the value of γ is taken to be $\gamma = 1.4$ for diatomic gases. The value for $\beta_{\rm dia}^*$ obtained by Eucken is 1.94. The closeness of these numbers can be taken as an indication of the correct approach. For a van der Waals gas the translational energy will have an extra term that is independent of temperature, which will give the same Eucken number. This could be caused by the fact that the statistical formalism of a diatomic gas takes into account the effects of the van der Waals gas model. For example, the fixed distance between the two point particles generates over time a spherically symmetric shape when all of the rotations are considered. This spherically symmetric shape resembles the volume of a monoatomic van der Waals gas molecule. In addition, the van der Waals gas considers pair potentials, which is the same type of potential that is considered when one deals with the statistical description of diatomic gases.

Appendix: Internal Energy in Exponential Form

In general, the average internal energy is given by

$$\langle E^{\text{int}} \rangle = \langle E^{\text{kin}} \rangle + \langle E^{\text{pot}} \rangle$$
 (A1)

Because setting $W(r) = W(r_m)$ indicates negligible kinetic energy caused by radial motion, the value of $\langle E^{\text{kin}} \rangle$ equals $k_B T$ at equilibrium and local equilibrium as well. The value of $\langle E^{\text{pot}} \rangle$ is expected to be a multiple of $k_B T$, and one can write

$$\langle E^{\text{int}} \rangle = \langle E^{\text{kin}} \rangle + q \langle E^{\text{kin}} \rangle \tag{A2}$$

where $\langle |E^{\text{pot}}| \rangle = q \langle E^{\text{kin}} \rangle$. If one writes

$$q = \sum_{\ell=1}^{\infty} [\beta W(r_m)]^{\ell} / \ell$$

and chooses the Lennard-Jones potential $W(r_m) = -0.77k_BT_c$, one gets q = 0.537. Therefore, assuming small oscillations about r_m , one gets $\langle E^{\text{kin}} \rangle = k_B T_c$, which will lead to $\langle |E^{\text{pot}}| \rangle = 0.537 k_B T_c$, which is about the average energy contribution from a harmonic oscillator. This is consistent with our assumption to set $W(r) = W(r_m)$, which states that the two particles may be in the neighborhood of a fixed equilibrium distance. Therefore, for temperatures in the neighborhood of T_c , Eq. (A2) can be written as

$$\langle E^{\text{int}} \rangle = \langle E^{\text{kin}} \rangle \exp[\beta W(r_m)] \equiv \langle E^{\text{int}}(v) \rangle \exp[\beta W(r_m)]$$
 (A3)

From Eq. (A3) one gets $E^{\text{int}}(v, r_m) = E^{\text{int}}(v) \exp[\beta W(r_m)]$. The equation

$$\int_{\Gamma} d^3r g(r_m)$$

can be integrated to give

$$\Gamma g(r_m) = 1/n \tag{A4}$$

Acknowledgments

Gratitude is acknowledged to Ronald B. Guenther and Ernest L. Roetman for their important follow-up and evaluation of this work.

References

¹Ali, A. H., "Statistical Mechanical Derivation of Cattaneo's Heat Flux Law," Journal of Thermophysics and Heat Transfer, Vol. 13, No. 4, 1999, pp. 544-546.

Hirschfelder, J. O., Curtiss, C. F., and Bird, R. B., Molecular Theory of

Gases and Liquids, Wiley, New York, 1954, pp. 32, 245, 454, 498.

³Singwi, K. S., Tosi, M. P., Land, R. H., and Sjölander, A., "Electron Correlations at Metallic Densities," Physical Review, Vol. 176, 1968, pp. 589-

⁴Chandler, D., Introduction to Modern Statistical Mechanics, Oxford Univ. Press, New York, 1987, pp. 195-201.

⁵ Hansen, J. P., and McDonald, I. R., *Theory of Simple Liquids*, Academic, Orlando, FL, 1986, pp. 18, 67.

⁶Tien, C. L., and Lienhard, J. H., Statistical Thermodynamics, Holt, Rinehart, and Winston, Philadelphia, 1971, pp. 311-313.

⁷ Jeans, J. H., The Dynamical Theory of Gases, Dover, New York, 1954, pp. 184-186, 195.

Thermal Contact Conductance of Metal/Polymer Joints

J. J. Fuller* and E. E. Marotta[†] Clemson University, Clemson, South Carolina 29634-0921

Introduction

POLYMERS and organic materials are being employed to a greater extent in power generating systems, and with greater use follows an increased interest in the thermal transport properties of polymers. These properties include thermal conductivity, heat capacity, and the thermal contact conductance at the interface with other materials. One important consideration where limited knowledge exists is the heat flow across a metal/polymer interface. Currently, a usable and verifiable model does not exist for predicting the thermal performance of metal/polymer joints.

Marotta and Fletcher¹ measured the thermal conductivity and the thermal contact conductance of several widely available thermoplastic and thermosetting polymers. They compared the experimentally measured data with the current thermal contact models developed for metal/metal contact, such as the elastic contact model developed by Mikic² and the plastic contact model developed by Cooper et al. (CMY).3 The Mikic and CMY models are accepted and proven for metal/metal contacts, but it was observed that a new thermal contact model was needed for a metal in contact with a much softer polymer layer with either finite or infinite length (half-space solution).

Problem Statement

The goal was to obtain a verifiable and usable analytical model for the prediction of thermal joint resistance between a metal and a polymer. The scope of this investigation was limited to assuming

Received 17 May 1999; presented as Paper 99-3490 at the AIAA 33rd Thermophysics Conference, Norfolk, VA, 28 June-1 July 1999; revision received 1 October 1999; accepted for publication 11 October 1999. Copyright © 2000 by J. J. Fuller and E. E. Marotta. Published by the American Institute of Aeronautics and Astronautics, Inc., with permission.

^{*}Research Assistant, Department of Mechanical Engineering. Member AIAA.

[†]Assistant Professor, Department of Mechanical Engineering. Member AIAA.